# **RCEM 2019**

THE 11TH SYMPOSIUM ON RIVER, COASTAL AND ESTUARINE MORPHODYNAMICS

## **BOOK OF ABSTRACTS**



AUCKLAND, NEW ZEALAND 16<sup>TH</sup>-21<sup>ST</sup> NOVEMBER 2019





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#### Bottom stress and hydrodynamics: field study on Perkpolder (NL)

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#### 1. Introduction

A big part of The Netherlands territory is below sea level; for this reason, a lot of lands have been reclaimed through the years by means of the creation of polders. However, this process caused the loss of intertidal areas, that are essential for the safeguard of natural habitats. From the last century the European governments provided the depoldering of some areas. The study area (Perkpolder, NL, located in the Western Scheldt) it is one of these pilot locations. The morphology and the evolution of the entire area and of the channels network have been influenced, over the last four years (since the tidal basin was created), by the local tidal conditions inside the basin. These conditions, in turn, determine the flux of sediment, nutrients and biota. With the aim to evaluate the hydrodynamic condition and its effects on sediment transport in the Perkpolder area, water velocity and depth have been continuously measured in six different locations in the Perkpolder area, four in the channels and two in the mudflat

### 2. Bed Shear Stress (BSS) and critical bed shear stress calculation

Starting from the velocity measurements, the BSS and the critical values of the BSS, on both mudflat and channels, have been evaluated according to two different approaches suggested by van Rijn: the formula used for the BSS is (van Rijn, 1984):

$$\tau(t) = \frac{\rho}{c^2} \bar{u}(t)^2 \tag{1}$$

Where  $\rho$  is the density,  $\bar{u}$  is the horizontal velocity averaged on the vertical and *c* is the adimensional Chézy coefficient, while the critical values of the BSS have been calculated by taking into account the cohesion and the packing effect, as explained in the formulas (van Rijn, 2007):

$$au_{cr,bed,fine} = \left(\frac{d_{sand}}{d_{50}}\right)^{0.5} au_{cr,0}$$
 (2)

$$\tau_{cr,bed,sand} = (1 + p_{cs})^3 \tau_{cr,0}$$
 (3)

$$d_{50} > 62\mu m \qquad \tau_{cr,bed} = (1 + p_{cs})^3 \tau_{cr,0} \tag{4}$$

Where  $d_{sand} = 62\mu m$ ,  $p_{cs}$  is the percentage of clay and silt and  $\tau_{cr,0}$  is the critical BSS calculated without considering the cohesion and the packing effects. The values as obtained have been compared to evaluate the sediments transport capacity of the water flow.

#### 3. Tidal Phase Prevalence Index (TPPI)

To have a better qualitative factor, that allows to compare the impact of the water flow, both in ebb and flood phase, and the behaviour of the different cross sections, a new parameter has been introduced.

This parameter is called "Tidal Phase Prevalence Index" (TPPI) and it is expressed through the following equations:

for 
$$\theta > \theta_{cr}$$
  $TPPI = \frac{1}{T/2} \int_0^{T/2} (\theta - \theta_{cr}) dt$  (5)

for 
$$\theta < \theta_{cr}$$
  $TPPI = 0$  (6)

Where T is the tidal period,  $\theta$  is the Shields parameter and  $\theta_{cr}$  is the critical Shields parameter.

Since  $\theta_{cr}$  and, consequently, the TPPI value depends on the equivalent *Nikuradse roughness*  $K_s$ , a sensitivity analysis has been carried out changing the value of  $K_s$ . In the table below the TPPI values calculated with the  $K_s$ 

The table below the TPP1 values calculated with the  $K_s$  value suggested by van Rijn are reported:

Moasur	$d_{50} < d_{sand}$				$d_{50} > d_{sand}$	
ement	TPPI	TPPI	TPPI	TPPI		
Point	fine flood				flood	TPPI ebb
BC3_1	0.323	0.301	0	0	NA	NA
AC3_1	0.23	0.214	0	0	NA	NA
BC4_1	NA	NA	NA	NA	0.002	0.002
AC2_1	NA	NA	NA	NA	0	0
MC2_1	NA	NA	NA	NA	0	0
MC2_2	0.009	0.007	0	0	NA	NA
	Point   BC3_1   AC3_1   BC4_1   AC2_1   MC2_1	ement PointTPPI fine floodBC3_10.323AC3_10.23BC4_1NAAC2_1NAMC2_1NA	TPPI fine floodTPPI fine ebbBC3_10.3230.301AC3_10.230.214BC4_1NANAAC2_1NANAMC2_1NANA	TPPI ement PointTPPI fine floodTPPI sand ebbTPPI sand floodBC3_10.3230.3010AC3_10.2330.2140BC4_1NANANAAC2_1NANANAMC2_1NANANA	ement PointTPPI fine floodTPPI fine ebbTPPI sand floodPPI eblBC3_10.3230.30100AC3_10.2330.21400BC4_1NANANANAAC2_1NANANANAMC2_1NANANANA	TPPI pointTPPI fine floodTPPI fine ebbTPPI sand floodTPPI ebbBC3_10.3230.30100NAAC3_10.230.21400NABC4_1NANANANA0.002AC2_1NANANANA0MC2_1NANANANA0

Table 1: TPPI values

#### 4. Conclusions

The bed shear stress results much higher in the channels than on the mudflat. The sediment dynamic on the mudflat are dominated by deposition, whereas in the channels are governed by erosion, and it is in agreement with the observed morphological evolution. Mudflat and channels, are still getting modified by the action of the water, making difficult the vegetation engraftment. TPPI gives a qualitative indication about erosion-deposition rate TPPI values confirm that the intertidal basin is characterized by a flood dominance.

#### References

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