

# 8<sup>th</sup> IAHR EUROPE CONGRESS

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## Dam break in power-law cross-section channels with different upstream/downstream widths

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### ABSTRACT

The dam break problem is studied in a channel characterised by a power-law cross-section, with different widths upstream and downstream of the dam. This research is the extension of a previous study by Valiani and Caleffi (2019), designed for rectangular cross-sections, to different and more complex geometries. A 1D a-SWE (one dimensional *augmented* Shallow Water Equation) system is developed, which has been shown to capture the full range of possible solutions.

To address abrupt changes in the section, the classic SWE system is augmented with a third equation consisting of the time-invariance of the width scale. The idea of the augmented system was introduced by LeFloch and Thanh (2011) for the unit-width SWE, using the bed elevation as an additional variable, and by Valiani and Caleffi (2019) for rectangular narrowing/widening cross-sections, using the channel width as an additional variable.

The numerical model is a Finite Volume Method, second-order accurate in space and time, using a path conservative scheme to evaluate the numerical flux at the cell interfaces. A nonlinear path is adopted, which is shown to be optimal for capturing both the sharp contact wave at the dam and the moving shock(s) downstream of the dam.

The comparison of the numerical results with the analytical results for different solution patterns of the solution supports the confidence in the reliability of the model.

### 1. Mathematical Model

We consider a channel with a power-law cross section, characterised by the following geometry:

$$b = b_0 \left(\frac{Y}{Y_0}\right)^m ; A = \frac{b_0 Y_0}{1+m} \left(\frac{Y}{Y_0}\right)^{1+m} ; I = \frac{b_0 Y_0^2}{(1+m)(2+m)} \left(\frac{Y}{Y_0}\right)^{2+m} \quad (1)$$

where  $b_0$  is the width scale,  $Y_0$  is the depth scale,  $m$  is the shape coefficient,  $b$  is the current width,  $Y$  is the current depth,  $A$  is the wetted area,  $I$  is the static moment of the cross section (Valiani and Caleffi, 2009).

A discontinuous width scale is considered, specifically  $b_{0L}$  upstream of the dam and  $b_{0R}$  downstream. Both cases of contraction and expansion cases are analysed.  $Y_L$  and  $Y_R$  ( $< Y_L$ ) are the initial upstream and downstream depths. The water is initially at rest everywhere. The 1D a-SWE system governing the problem is:

$$\begin{aligned} \frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} &= 0 \\ \frac{\partial Q}{\partial t} + \left[ \left(g \frac{A}{b}\right) - \left(\frac{Q^2}{A^2}\right) \right] \frac{\partial A}{\partial x} + \left(2 \frac{Q}{A}\right) \frac{\partial Q}{\partial x} - \left(g \frac{A}{b}\right) \Lambda \frac{\partial K}{\partial x} &= 0 \\ \frac{\partial K}{\partial t} &= 0 \end{aligned} \quad (2)$$

where  $(x, t)$  are space and time, respectively;  $Q$  is the discharge,  $g$  is the acceleration due to gravity,  $K$  is the additional geometrical variable ( $b_0$  in this specific case), and  $\Lambda$  is a geometrical variable ( $A/b_0$  in this specific case), whose definition ( $\eta$  is the water surface elevation) is:

$$\Lambda \frac{\partial K}{\partial x} = \left( \frac{\partial A}{\partial x} \right)_{\eta=const} \quad (3)$$

Such a term is crucial when geometric discontinuities occur but vanishes in smooth cases.

## 2. Numerical Model

Numerical integration is performed using a second-order accurate Finite Volume Method, with a DOT (Dumbser and Toro, 2011) Riemann solver to compute the flux at the cell boundaries, where the solution is discontinuous (Toro, 2009). A path-conservative scheme (Dal Maso et al., 1995; Castro et al., 2008) is employed; the linear path introduced by Parés (2006) is modified here as proposed in Valiani & Caleffi (2019), introducing an original nonlinear path that can be adopted for cross-sections of arbitrary shape.

Referring to cell  $i$ , its boundaries are  $x_{i-1/2}$  and  $x_{i+1/2}$ . At this last boundary, each state variable  $W$  has two different values,  $W_{i+1/2}^-$ ,  $W_{i+1/2}^+$ , on the left and right respectively. We assume a linear path in the variables  $H$ ,  $Q$ ,  $K$ , where  $H$  is the total head of the flow:

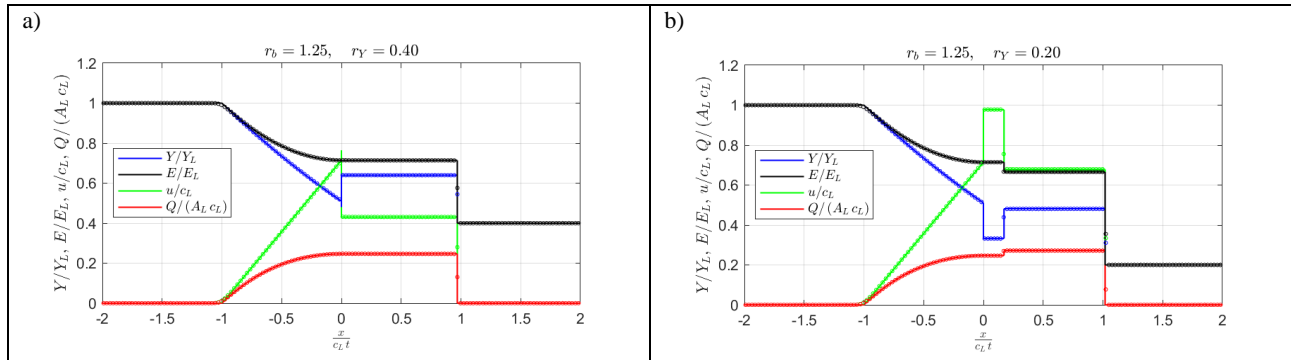
$$\begin{aligned} \Psi_H(H_{i+1/2}^-, H_{i+1/2}^+; s) &= H_{i+1/2}^- + (H_{i+1/2}^+ - H_{i+1/2}^-) s \\ \Psi_Q(Q_{i+1/2}^-, Q_{i+1/2}^+; s) &= Q_{i+1/2}^- + (Q_{i+1/2}^+ - Q_{i+1/2}^-) s \\ \Psi_K(K_{i+1/2}^-, K_{i+1/2}^+; s) &= K_{i+1/2}^- + (K_{i+1/2}^+ - K_{i+1/2}^-) s \end{aligned} \quad 0 \leq s \leq 1 \quad (4)$$

and a nonlinear path for the cross-sectional area,  $\Psi_A(A_{i+1/2}^-, A_{i+1/2}^+; s)$ , which must be derived from:

$$H(s) = \eta(s) + \frac{[Q(s)]^2}{2g[A(s)]^2}, \quad 0 \leq s \leq 1 \quad (5)$$

## 3. Results

Depending on the ratios  $b_{0R}/b_{0L}$  and  $Y_R/Y_L$ , 6 different solution patterns are possible (2 for contractions and 4 for expansions). There is a contact wave occurs at the dam position, and one (or more) shocks downstream of the dam. The augmented system approach is crucial to capture the correct solution when the resonant case (two eigenvalues are both zero) occurs at the dam position. The proposed numerical method gives excellent results for the whole range of cases considered. Examples are shown in Fig. 1.



**Fig. 1.** Dam break in power-law cross-sections for a sudden expansion,  $b_{0R}/b_{0L} = 1.25$ , for different initial depth ratios: a)  $Y_R/Y_L = 0.40$ ; b)  $Y_R/Y_L = 0.20$ . Lines/dots are analytical/numerical solutions.  $c$  is the relative celerity of small waves,  $E$  is the specific energy ( $=H$  for horizontal flat bed),  $u$  is the mean velocity; the subscript  $L$  is the initial reference value upstream of the dam.

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